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GIAN LUIGI CASALONE, CARLA MARIANI, ANGELO
MUGNOLI, MASSIMO SIMONETTA

**Crystal, Molecular and Electronic Structure of
1,1-diaryl-2-halogenoetkylenes. - II. Crystal and
Molecular Structure of
2-bromo—1,1-diphenyl-prop—1—ene**

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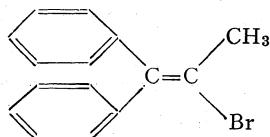
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Strutturistica chimica. — Crystal, Molecular and Electronic Structure of 1,1-diaryl-2-halogenoethylenes. — II. Crystal and Molecular Structure of 2-bromo-1,1-diphenyl-prop-1-ene^(*). Nota di GIAN LUIGI CASALONE, CARLA MARIANI, ANGELO MUGNOLI e MASSIMO SIMONETTA, presentata^(**) dal Corrisp. M. SIMONETTA.

RIASSUNTO. — La struttura cristallina del 2-bromo-1,1-difenil-prop-1-ene $C_{15}H_{13}Br$ è stata determinata a temperatura ambiente con metodi tridimensionali e affinata con un processo di minimi quadrati a matrice completa con fattori termici anisotropi. Il valore finale dell'indice R è 8,5%. Nella cella monoclinica, di parametri $a = 5,97$; $b = 16,97$; $c = 12,63 \text{ \AA}$; $\beta = 103,7^\circ$, gruppo spaziale P_{21}/c , sono presenti quattro molecole. In ciascuna di esse gli atomi sono distribuiti su tre piani: il piano etilenico e quelli dei due anelli benzenici, che risultano ruotati, rispetto al primo, di $70,7^\circ$ (anello in *trans* al bromo) e di $47,2^\circ$ (anello in *cis* al bromo). La distanza C—Br è $1,92 \text{ \AA}$.

The investigation of the crystal, molecular and electronic structure of 1,1-diaryl-2-halogenoethylenes has been undertaken in our laboratory [1].

The second compound investigated was 2-bromo-1,1-diphenyl-prop-1-ene, $C_{15}H_{13}Br$, m. p. $49^\circ C$:



which crystallizes from glacial acetic acid in transparent needles. The unit cell dimensions were determined from rotation and Weissenberg films, using $CuK\alpha$ radiation.

CRYSTAL DATA.

2-bromo-1,1-diphenyl-prop-1-ene.

$C_{15}H_{13}Br$ F. W. 273.2

Monoclinic, $a = 5.97 \pm 0.01$, $b = 16.97 \pm 0.02$, $c = 12.63 \pm 0.01 \text{ \AA}$, $\beta = 103.7 \pm 0.1^\circ$, with λ ($CuK\alpha_1$) = 1.5405 , λ ($CuK\alpha_2$) = 1.5443 , λ ($CuK\alpha$) = 1.5418 \AA ; $V = 1243.2 \text{ \AA}^3$; $D_m = 1.44 \text{ g. cm}^{-3}$ (by flotation); $Z = 4$; $D_e = 1.46 \text{ g. cm}^{-3}$; $F(000) = 552$; Absorption coefficient for $CuK\alpha$ radiation, 43.9 cm^{-1} .

(*) Work done at the Institute of Physical Chemistry – University of Milan, Milan, Italy.

(**) Nella seduta del 12 novembre 1966.

Space group P₂₁/c (No. 14), from systematic absences: $h \parallel l$ if $l = 2n + 1$, $o \parallel k \parallel o$ if $k = 2n + 1$.

INTENSITY MEASUREMENTS.

The X-ray intensities were estimated visually from sets of multiple-film equi-inclination Weissenberg photographs taken at room temperature about the α axis (6 layers) using a crystal with cross section of $0.19 \times 0.25 \text{ mm}^2$. From a total number of 2850 possible independent reflections for CuK α radiation, 2445 were collected, of which 591 were too low to be observed. The intensities were scaled together within the same layer following Rae [2] and then corrected for Lorentz, polarization and spot-size [3] factors. An evaluation of the σ for each individual observation was obtained from a statistical analysis [4]. A preliminary scaling of the data belonging to different layers was made after the structure was solved, by comparison between the F_o and F_c values; the individual scaling factors for each layer were subsequently refined in the least-squares process. No absorption or extinction correction was applied. Atomic scattering factors were calculated by means of analytical expressions following [5] for bromine and carbon, and [6] for hydrogen atoms.

STRUCTURE DETERMINATION AND REFINEMENT.

The first step in the solution of the structure was the interpretation of the $P(v, w)$ Patterson projection. This enabled us to recognize the y, z coordinates of the bromine and of all the carbon atoms. A generalized Patterson synthesis [7] gave two possible x coordinates for the bromine atom; considering all the geometries of the molecule consistent with the okl projection, by comparison between observed and calculated structure factors within each layer the correct set of x coordinates for the bromine and all the carbon atoms was deduced. At this stage of the research, a structure factor calculation gave an overall reliability index $R = 21\%$.

A first isotropic refinement was done by a few cycles of block-diagonal least-squares, which lowered the R index to 16%. The final refinement was achieved by four cycles of full-matrix least-squares, in which anisotropic temperature factors were adopted for each atom in the structure, except for hydrogen atoms. These latter were omitted from the least-squares refinement, being introduced only in the structure factor calculations. Benzenic hydrogen atoms were assumed to lie on the line bisecting the angle between the two bonds from the same carbon atom, with carbon-hydrogen bond distances equal to 1.08 \AA . To these atoms an isotropic temperature factor $B = 4 \text{ \AA}^2$ was assigned. The positions of the hydrogen atoms of the methyl group were not determined.

The quantity minimized in the least-squares calculations was $\Sigma w (F_o - |kF_c|)^2$, the weights w being derived from the σ 's of each single observation, as determined in the data reduction process. After the final cycle, all the shifts were below one half of the corresponding e.s.d. Unobserved reflections were assigned a threshold value based on the lowest observable intensity, and introduced in the refinement only when $|kF_c|$ exceeded this value. The final R index is 8.5 % for the observed reflections.

Table I gives the final atomic coordinates with their e.s.d.'s. Anisotropic temperature factors with their e.s.d.'s are listed in Table II. The numbering of the atoms is included in fig. 1 and 2. Structure factors based on the final parameters are compared with the observed structure amplitudes in Table III.

TABLE I.
Final coordinates with standard deviations ($\times 10^4$).

ATOM	x/a	y/b	z/c	ATOM	x/a	y/b	z/c
Br	.1470 (1)	.1531 (<1)	.0329 (1)	C(13)	.2822 (16)	.4931 (4)	.3477 (5)
C(1)	.0552 (11)	.2158 (3)	.2297 (4)	C(14)	.4802 (14)	.4518 (5)	.3459 (5)
C(2)	.1709 (11)	.2385 (3)	.1348 (4)	C(15)	.4753 (11)	.3921 (4)	.2746 (5)
C(3)	.2706 (10)	.3050 (3)	.1211 (4)	H(1)	.5851	.2187	.0418
C(4)	.3881 (11)	.3255 (3)	.0335 (4)	H(2)	.7931	.2608	—.0945
C(5)	.5502 (12)	.2758 (4)	.0038 (5)	H(3)	.7084	.3895	—.1848
C(6)	.6658 (13)	.2991 (5)	—.0735 (6)	H(4)	.4253	.4761	—.1372
C(7)	.6186 (15)	.3715 (5)	—.1240 (6)	H(5)	.2156	.4360	.0004
C(8)	.4609 (14)	.4196 (4)	—.0975 (5)	H(6)	—.0891	.3965	.1481
C(9)	.3431 (11)	.3971 (4)	—.0192 (5)	H(7)	—.0811	.5049	.2774
C(10)	.2729 (11)	.3699 (3)	.2011 (4)	H(8)	.2881	.5410	.4046
C(11)	.0715 (13)	.4122 (4)	.2039 (6)	H(9)	.6406	.4673	.4020
C(12)	.0750 (14)	.4731 (4)	.2762 (6)	H(10)	.6329	.3608	.2747

The average planes in the molecule were determined as described in [8]. In Table IV the results for three planes are summarized—the planes of the two phenyl rings, *trans* and *cis* with the bromine atom (both including the C(3) atom), and the plane of the molecular skeleton, as defined by the atoms C(2), C(3), C(4), C(7), C(10), C(13). In all the three cases the distances between any atom and the involved plane are of the same order of the correspond-

ing σ_1 (standard deviation for the position along the direction perpendicular to the plane). The bromine atom and the methyl carbon atom lie at 0.07 Å apart from the molecular skeleton plane.

TABLE II.

Thermal exponent coefficients (with e.s.d.'s); b_{ij} as given here are defined by:

$$T = \exp [-10^{-4} (b_{11} h^2 + b_{22} k^2 + b_{33} l^2 + 2 b_{12} hk + 2 b_{13} hl + 2 b_{23} kl)]$$

ATOM	b_{11}	b_{22}	b_{33}	b_{12}	b_{13}	b_{23}
Br	480 (124)	28 (<1)	92 (1)	-12 (1)	69 (1)	-6 (<1)
C(1)	249 (126)	33 (2)	48 (3)	-6 (5)	51 (7)	8 (2)
C(2)	259 (124)	27 (2)	48 (3)	12 (5)	28 (7)	4 (2)
C(3)	165 (125)	28 (2)	40 (3)	0 (5)	20 (6)	3 (2)
C(4)	167 (127)	28 (2)	48 (3)	10 (5)	23 (6)	0 (2)
C(5)	212 (128)	45 (3)	59 (4)	10 (7)	30 (8)	-2 (3)
C(6)	209 (124)	56 (4)	86 (5)	29 (7)	63 (9)	5 (3)
C(7)	394 (131)	56 (3)	67 (5)	-50 (9)	82 (10)	4 (3)
C(8)	452 (127)	30 (2)	61 (4)	-16 (7)	64 (9)	4 (2)
C(9)	262 (125)	34 (2)	49 (4)	-5 (6)	37 (7)	5 (2)
C(10)	265 (125)	28 (2)	41 (3)	-6 (5)	40 (7)	6 (2)
C(11)	260 (124)	39 (3)	81 (5)	12 (6)	58 (9)	-6 (3)
C(12)	449 (129)	26 (2)	85 (5)	-6 (6)	69 (11)	-2 (3)
C(13)	549 (129)	38 (3)	59 (4)	-32 (8)	91 (11)	0 (3)
C(14)	374 (127)	47 (3)	51 (4)	-40 (8)	13 (9)	-6 (3)
C(15)	213 (125)	41 (2)	44 (3)	-18 (6)	15 (7)	0 (2)

Bond distances and bond angles are reported in fig. 1 and fig. 2, where the molecule is drawn referred to an orthogonal right-handed coordinate system X' Y' Z' whose Y' Z' plane is the average plane of the molecular skeleton previously described. The average value of the e.s.d.'s [9, 10] is 0.009 Å for the bond distances and 0.5° for the bond angles. Both the phenyl rings are rotated with respect to the molecular skeleton plane, the dihedral angles being $\vartheta_1 = 70.7^\circ$ and $\vartheta_2 = 47.2^\circ$ for the ring *trans* and *cis* to the bromine atom, respectively.

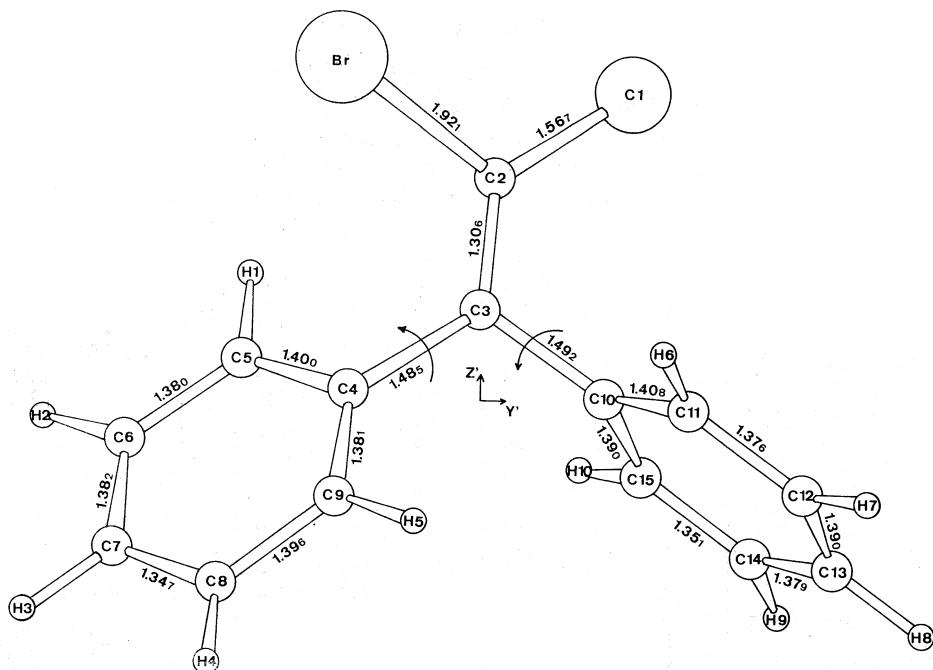


Fig. 1. – Bond lengths (\AA) in the crystal. The average e.s.d. is 0.009 \AA .

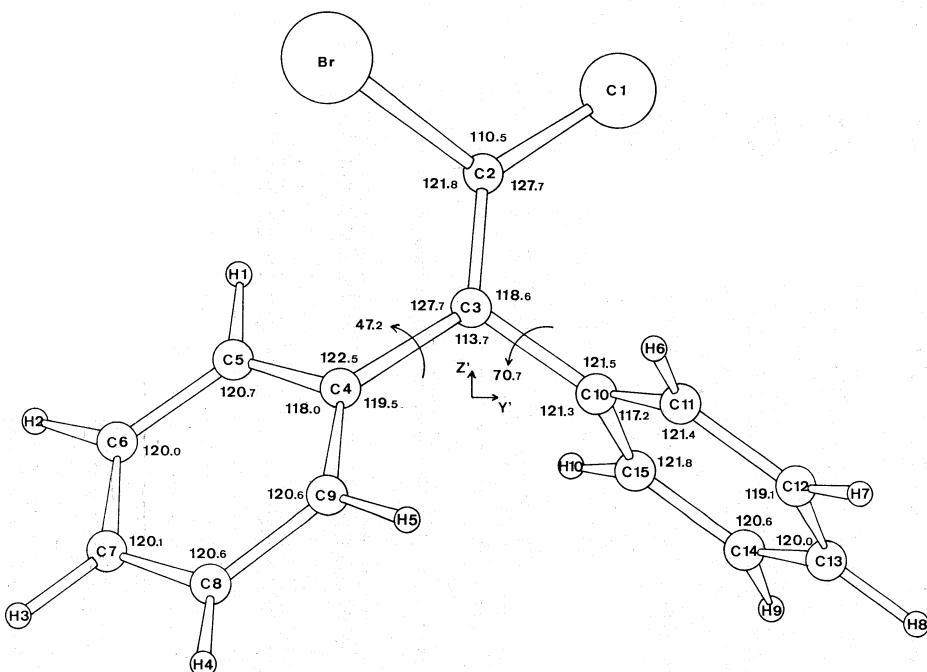


Fig. 2. – Bond angles (degrees) in the crystal. The average e.s.d. is 0.5° .
Both the phenyl rings are rotated with respect to the average plane of the molecular skeleton (see text).

TABLE III⁽¹⁾.

Observed and calculated structure factors. Each group of three columns contains in order l , $|F_o|$ and $|F_c|$.

A minus sign before the $|F_o|$ value designates unobserved reflection. Reflections indicated by an asterisk were given zero weight in the least-squares refinement and excluded from the R calculation.

\emptyset	\emptyset	l	7	91	57	6	195	205	8	236	-235
*2	572	867	8	80	-72	7	321	299	9	37	38
4	640	710	9	113	109	8	106	-99	10	59	-54
6	327	326	10	163	166	9	356	331	11	28	-38
8	252	225	11	139	135	10	217	-212	12	71	-85
10	111	-108	12	73	-73	11	104	103	13	87	85
12	235	-252	13	85	86	12	130	-145	14	-15	-13
14	35	-35	14	94	83	13	52	61			
			15	94	100	14	117	-116	Ø	10	L
\emptyset	I	L	Ø	4	L	Ø	7	L	Ø	414	-437
1	238	268	Ø	4	L	Ø	7	L	1	42	41
2	436	-536	*Ø	645	-881	*1	901	1094	2	577	-620
3	132	170	1	607	593	2	68	-69	3	91	-64
4	295	-359	2	675	-751	3	655	730	4	295	-292
5	317	325	3	148	-57	4	478	-510	5	104	89
6	596	-653	4	601	-651	5	261	251	6	204	-215
7	73	57	5	426	446	6	280	-253	7	52	56
8	449	-470	6	117	-99	7	80	64	8	73	69
9	184	-167	7	356	362	8	217	-201	9	68	-61
10	362	-374	8	158	157	9	91	-74	10	154	154
11	217	-215	9	186	196	10	221	-221	11	28	24
12	134	-111	10	-30	-20	11	37	-40	12	104	99
13	68	67	11	-30	-7	12	139	-143	13	45	38
14	24	42	12	195	207	13	63	-78			
15	94	-91	13	39	-25	14	43	-39	Ø	11	L
			14	124	122				I	408	-400
Ø	2	L	15	52	53	Ø	8	L	2	299	298
Ø	568	-567	Ø	5	L	Ø	289	272	3	163	-159
1	204	226	Ø	5	L	I	91	71	4	371	354
*2	653	-934	I	243	226	2	184	-130	5	35	-31
*3	855	-1208	2	506	547	3	336	-324	6	423	446
4	391	-346	3	391	-336	4	139	107	7	37	26
5	577	-678	4	544	621	5	430	-444	8	353	342
6	-21	-11	5	292	237	6	108	99	9	52	40
7	410	-421	6	659	743	7	434	-441	10	204	208
8	111	-115	7	-26	II	8	-30	17	II	122	111
9	358	-396	8	469	478	9	233	-232	12	50	49
10	-30	22	9	78	55	10	47	-38	13	63	53
11	146	-140	10	212	200	11	165	-169			
12	111	105	11	-30	-6	12	47	-54	Ø	12	L
13	128	-134	12	134	142	13	28	-17	Ø	238	241
14	54	39	13	-26	7	14	-17	33	I	323	306
15	-19	3	14	54	44	Ø	9	L	2	386	382
Ø	3	L	Ø	6	L	I	596	-637	3	252	232
I	210	-264	Ø	541	654	2	148	-166	4	165	144
2	466	506	I	43	27	3	513	-523	5	332	335
*3	829	-1105	2	699	794	4	508	-494	6	148	138
4	176	-170	3	567	552	5	254	-257	7	204	176
5	345	-360	4	386	425	6	367	-347	9	245	241
6	377	-363	5	56	67	7	167	-148	10	50	-47

(1) Note added in proofs. In this Table, a transcription of a computer output, the symbol \emptyset means zero, and L means l .

Segue: TABLE III.

II	108	97	Ø	17	L	I	I	L	I2	—34	—Ø
I2	—19	—25	I	215	—226	—15	37	—43	I3	—32	5
I3	—13	—19	2	52	47	—14	155	143	I4	—26	18
			3	241	—263	—13	—32	—2			
Ø	13	L	4	143	149	—12	190	219	I	3	L
I	513	562	5	143	—152	—11	69	61	I5	—22	—2
2	—28	11	6	102	104	—10	311	331	—14	30	43
3	317	348	7	24	35	—9	273	273	—13	27	5
4	43	—39	8	82	79	—8	—27	35	—12	69	69
5	130	132	9	52	41	—7	273	281	—11	54	55
6	128	114				—6	54	42	—10	34	27
7	115	118	Ø	18	L	—5	518	515	—9	291	—290
8	71	—78	Ø	—28	—17	—4	357	—303	—8	261	247
9	82	—81	I	63	61	—2	293	170	—7	680	—737
IØ	37	28	2	43	54	—1	205	244	—6	42	37
II	154	—140	3	139	127	*Ø	796	—1324	—5	656	—708
I2	—17	—10	4	87	91	*1	775	1056	—4	447	—436
			5	228	242	*2	844	—1107	—3	708	—804
Ø	14	L	6	69	68	3	279	231	*—1	940	—1180
Ø	271	267	7	215	210	4	519	—550	Ø	445	—462
I	124	—105	8	52	41	5	481	—388	*1	780	—1007
2	228	223				6	498	—496	2	730	—729
3	236	—237	Ø	19	L	7	219	—214	3	330	—311
4	113	95	I	236	223	8	156	—144	4	496	—488
5	186	—154	2	76	80	9	126	—115	5	195	199
6	—30	13	3	104	107	10	122	—96	6	211	—167
7	182	—167	4	73	62	11	66	—81	7	248	229
8	54	—58	5	108	99	12	182	195	8	68	57
9	165	—167	6	56	48	13	169	—149	9	379	370
IØ	—24	—29				14	—26	23	IØ	116	—113
II	115	—108	7	—15	—3				I1	123	115
I2	—13	—22							I2	60	—60
			Ø	20	L	I	2	L	I3	160	128
Ø	15	L	Ø	207	166	—15	101	99	I4	—23	—29
I	130	—134	I	21	—25	—14	—30	7			
2	128	—114	2	210	181	—13	52	58	I	4	L
3	47	44	3	—21	8	—12	—34	37			
4	208	—196	4	69	61	—11	212	233	—15	37	—36
5	—30	—3	5	63	—70	—10	61	—64	—14	52	59
6	291	—310				—9	508	494	—13	77	—75
7	—28	18	Ø	21	L	—8	286	—258	—12	58	—64
8	172	—184	I	59	51	—7	360	352	—11	222	—235
9	69	—62	2	56	—58	—6	64	—83	—10	92	—87
IØ	130	—114				—5	496	432	—9	216	—215
II	30	32	I	Ø	L	—4	27	32	—8	137	—156
						*—3	554	—526	—7	248	—227
Ø	16	L	—14	163	—174	I	414	—532	—5	271	—252
Ø	341	—365	—12	—34	—34	Ø	334	—265	—4	256	—323
I	—30	—15	—10	229	214	I	622	—760	—3	385	380
2	289	—293	—6	553	565	2	735	793	*—2	970	—1164
3	99	—102	—4	1191	1227	3	519	—583	—1	259	314
4	315	—335	2	780	—936	4	361	359	Ø	60	—87
5	152	—155	4	23	—15	5	488	—505	I	820	941
6	52	—54	6	474	—462	6	51	34	2	332	—313
7	73	—66	8	353	—334	7	416	—394	3	596	645
8	—24	—5	IØ	319	—350	8	132	118	4	40	—25
9	—21	—24	12	200	—198	9	160	—139	5	588	609
IØ	35	27	14	—26	40	IØ	240	248	6	163	165
						I1	66	75	7	171	148

Segue: TABLE III.

8	342	328	4	266	-238	1	588	-655	Ø	456	-444
9	97	88	5	222	211	2	163	134	I	179	-138
I0	156	143	6	405	-388	3	756	-906	2	229	-210
I1	163	148	7	197	195	4	42	-50	3	222	192
I2	51	53	8	211	-202	5	445	-449	4	-34	31
I3	-29	42	9	66	-66	6	82	-70	5	148	148
I4	-23	15	10	185	-174	7	419	-411	6	279	273
			11	37	-43	8	-37	-14	7	51	54
I	5	L	12	140	-129	9	87	-77	8	305	282
-I5	23	-20	14	34	-43	11	-34	-16	9	58	56
-I4	116	-113				12	-32	-3	I0	163	172
-I3	-34	26	I	7	L	13	-23	I0	I2	105	106
-I2	205	-219				14	-16	I3	I3	-18	-8
-I1	58	-66	-15	55	-52				I	II	L
-I0	253	-257	-14	79	74	I	9	L			
-9	66	40	-13	63	-74				-I3	-23	16
-8	327	-371	-12	87	86	-14	-21	-15	-I2	145	-129
-7	185	-163	-11	-37	-10	-13	79	74	-I1	48	68
-6	263	-237	-10	-37	-12	-12	89	81	-I0	151	-163
-5	379	405	-9	68	59	-11	-37	5	-9	190	-207
-4	253	247	-8	142	159	-10	205	201	-8	227	-212
-3	390	-379	-7	359	373	-9	-37	-35	-7	74	-72
*-2	707	869	-6	105	-86	-8	448	457	-6	71	-70
-I	160	121	-5	678	770	-7	148	-149	-5	251	-262
Ø	648	730	-4	63	50	-6	48	-38	-4	-34	17
I	256	231	-3	641	649	-5	311	-318	-3	229	-220
2	682	807	-2	348	-347	-4	45	-22	-2	374	358
3	322	300	-1	259	291	-3	461	-468	-1	245	-212
4	815	914	Ø	293	-276	-2	195	-190	Ø	396	401
5	353	294	I	364	367	-1	377	-361	I	-32	-9
6	514	499	2	211	-189	Ø	433	-421			
7	156	-136	3	197	-188	I	51	-65	2	541	585
8	51	46	4	251	-249	2	322	-325	3	158	136
9	166	158	5	277	-248	3	100	-87	4	401	368
I0	105	101	6	60	-63	4	456	-431	5	45	-21
I1	114	-107	7	234	-238	5	82	58	6	216	210
I2	-34	-35	8	216	-214	6	123	-123	8	105	101
I3	66	71	9	287	-274	7	263	247	9	85	80
I4	74	-83	I0	129	128	8	153	-144	I0	-34	-21
			I1	160	-168	9	122	111	I1	26	49
I	6	L	I2	-32	17	I0	-37	26	I2	-23	14
			I3	142	-123	I1	89	I01	I3	-14	-13
-I5	48	-45	I4	40	52	I2	-29	27			
-I4	-29	-24				I3	79	73	I	I2	L
-I3	I00	-I00	I	8	L				-I3	I08	-I10
-I2	145	161	-I4	77	-76	I	I0	L	-I2	-26	7
-I1	122	-134	-I3	190	181	-I4	-18	16	-I1	190	-173
-I0	222	230	-I2	-34	12	-I3	-26	-32	-I0	60	65
-9	-37	-28	-I1	203	233	-I2	-32	I	-9	153	-156
-8	334	371	-I0	60	-59	-I1	-34	II	-8	177	173
-7	-32	4	-I0	203	203	-I0	122	-132	-6	66	-68
-6	541	580	-9	203	-203	-I0	122	-122	-6	297	306
-5	471	-474	-8	87	-72	-9	122	-122	-5	82	-84
-4	907	I005	-7	314	325	-8	403	-398	-4	234	222
-3	224	255	-6	51	48	-7	169	-157	-3	222	207
-2	664	725	-5	55	-47	-6	416	-403	-2	123	126
-I	345	328	-4	134	-119	-5	34	40	-I	366	348
Ø	527	557	-3	89	65	-4	530	-541	Ø	245	216
I	237	247	-2	182	168	-3	32	41	I	577	588
2	327	296	-I	530	-584	-2	664	-703	2	148	139
3	282	265	Ø	137	122	-I	48	21			

Segue: TABLE III.

3	405	422	8	74	-73	-3	177	-189	4	58	-57
4	105	-91	9	126	-122	-2	134	135	5	77	-94
5	279	267	10	123	-113	-1	145	-152			
6	-37	-21	11	-18	24	ø	97	97	1	21	L
7	242	244				1	89	-100			
8	129	-136				2	185	196	-4	-16	2
9	92	107	I	15	L	3	34	34	-3	51	43
10	92	-85	-11	51	-52	4	140	153	-2	89	-102
11	32	-44	-10	151	134	5	103	111	-1	-21	10
12	51	-46	-9	85	-73	6	140	133	ø	126	-124
			-8	114	123	7	174	165	I	-18	-7
I	13	L	-7	116	-119	8	60	54	2	148	-163
-13	-14	-12	-6	153	138				3	-16	-2
-12	-23	20	-5	58	-63	I	18	L	2	ø	L
-11	79	76	-4	-37	-2				-14	142	148
-10	-32	-2	-3	232	-228	-8	-21	3	-12	235	247
-9	158	170	-2	114	-116	-7	132	-114	-10	378	414
-8	82	-91	-1	229	-207	-6	29	-5	-8	626	610
-7	216	227	I	-37	-15	-4	32	-34	-6	440	453
-6	92	-83	2	308	-317	-3	119	108	-4	764	662
-5	374	377	3	-37	-24	-2	34	-38	-2	153	-97
-4	-37	-25	4	303	-320	-1	142	153	2	665	-721
-3	501	493	5	100	-99	ø	42	-36	4	111	-117
-2	97	-84	6	182	-188	I	205	232	6	528	519
-1	504	511	7	-34	-34	2	82	88	8	283	-266
ø	95	-84	8	37	-33	3	242	221	10	154	-168
I	156	168	9	51	48	4	-32	-42	12	-31	41
2	-37	-22	10	-21	-11	5	205	194	14	-18	-22
3	63	-43				6	32	-36			
4	-37	32				7	-21	23	2	I	L
5	137	-136	I	16	L	8	-16	17	-16	-17	8
6	37	-18	-10	-23	-7				-15	-23	2
7	100	-97	-9	82	74	I	19	L	-14	82	87
8	51	-54	-8	145	-149	-7	123	137	-13	30	43
9	126	-145	-7	89	75	-6	52	-55	-12	79	87
10	-29	23	-6	174	-187	-5	216	216	-11	44	31
11	137	-132	-5	-37	-15	-4	-29	-30	-10	-30	12
12	-14	-45	-4	287	-316	-3	190	182	-9	391	388
I	14	L	-3	129	-124	-2	29	44	-8	119	-117
-12	-18	-15	-2	158	-140	-1	148	139	-7	240	224
-11	122	118	-1	182	-174	ø	114	111	-6	44	-54
-10	-29	-ø	256	-263	I	29	36	-5	452	397	
-9	123	127	2	45	-32	2	163	127	-4	417	-357
-8	68	52	3	52	-46	3	71	82	-3	340	274
-7	68	70	4	142	-140	4	97	85	-2	746	-871
-6	245	254	5	77	-72	5	68	-57	*ø	790	-1032
-5	-37	8	6	123	134	6	82	75	I	226	-250
-4	300	304	7	-32	-21				2	162	-181
-3	58	39	8	132	131	I	20	L	3	515	-518
-2	197	189	9	52	46	-6	87	103	4	296	-257
-1	322	-318				-5	-21	4	5	69	-71
ø	219	196	I	17	L	-4	179	159	6	111	-103
I	290	-266				-3	-23	-34	7	265	-259
2	-37	32	-9	85	-86	-2	192	207	8	44	9
3	251	-254	-8	58	-43	-1	-26	-13	9	136	-114
4	-37	27	-7	151	-123	ø	111	102	10	139	149
5	224	-237	-6	89	-83	I	103	-98	11	69	-69
6	156	-167	-5	203	-201	2	85	79	12	64	63
7	160	-170	-4	103	119	3	-23	-21	13	-26	36
									14	-18	-39

Segue: TABLE III.

2	2	L	10	-36	35	7	175	-164	5	278	-260
-16	-14	18	11	136	141	8	-36	-46	6	-33	-13
-15	86	95	12	-31	20	9	-36	-41	7	355	-373
-14	-28	-35	13	-26	13	10	124	-133	8	100	103
-13	123	142				11	-33	-42	9	108	-93
-12	70	-82	2	4	L	12	98	-85	10	42	-8
-11	179	178	-16	-13	22	13	64	-60	11	44	-31
-10	182	-177	-15	80	-80	2	6	L	12	-26	18
-9	91	-73	-14	96	-92				13	46	-42
-8	129	-121	-13	80	-77	-15	51	-37			
-7	361	-343	-12	152	-165	-14	-28	33	2	8	L
-6	308	-294	-11	188	-193	-13	-31	-27	-14	28	-2
-5	711	-754	-10	129	-121	-12	96	93	-13	98	93
-4	411	-313	-9	93	-87	-11	72	73	-12	-33	-7
-3	934	-921	-8	268	-319	-10	108	103	-11	98	94
-2	79	-78	-7	175	168	-9	-36	-47	-10	57	75
*-1	860	-1070	-6	492	-550	-8	364	375	-9	-36	-22
Ø	281	285	-5	476	529	-7	-31	7	-8	232	242
*1	654	-812	-4	69	-86	-6	293	305	-7	64	49
2	60	-49	-3	525	633	-5	346	366	-6	-31	-7
3	647	-704	-2	160	153	-4	325	359	-5	485	-524
4	186	-169	-1	201	242	-3	469	520	-4	250	238
5	154	-130	Ø	178	170	-2	60	-50	-3	642	-692
6	54	45	I	657	730	-1	386	418	-2	150	125
7	90	96	2	217	234	Ø	479	-485	-1	667	-720
8	62	56	3	31	25	I	319	334	Ø	170	-165
9	180	173	4	618	679	2	72	-71	I	505	-546
10	80	81	5	136	133	3	392	368	2	64	-68
11	69	76	6	507	524	4	337	-327	3	329	-331
12	54	-62	7	-33	-27	5	-31	19	4	121	-112
13	108	102	8	124	119	6	242	-235	5	190	-198
14	-15	-4	9	-36	-27	7	96	76	6	186	-174
			Ø	126	117	8	240	-228	7	62	66
2	3	L	11	108	-118	9	160	-178	8	51	-48
-16	-14	28	12	80	64	10	54	-48	9	98	108
-15	-21	-23	13	103	-103	11	-31	-10	Ø	-33	-22
-14	-26	-8				12	-28	-26	11	62	65
-13	70	-64	2	5	L	13	-21	-24	12	-23	6
-12	133	147	-15	28	26						
-11	254	-269	-14	165	-150	2	7	L			
-10	-30	4	-13	-33	Ø	-15	49	57	2	9	L
-9	461	-485	-12	67	-67	-14	-26	22	-14	93	95
-8	231	226	-11	51	49	-13	72	49	-13	160	-137
-7	356	-403	-10	57	-59	-12	-33	-40	-12	186	145
-6	209	-182	-9	139	139	-11	311	352	-11	240	-222
-5	662	-615	-8	-33	5	-10	51	-47	-10	78	64
-4	56	-72	-7	-31	10	-9	350	381	-9	178	-175
-3	175	-182	-6	412	471	-8	85	-68	-8	162	-164
-2	191	-178	-5	72	-68	-7	374	375	-7	559	-619
-1	450	-375	-4	314	356	-6	39	-9	-6	335	-359
Ø	100	74	-3	88	105	-5	376	392	-5	304	-290
1	485	515	-2	603	727	-4	374	-389	-4	168	-169
2	186	159	-1	201	187	-3	335	322	-3	154	-151
3	744	799	Ø	469	543	-2	319	-302	-2	485	-497
4	69	-52	I	178	-149	-1	46	-48	-1	82	75
5	593	636	2	605	648	Ø	219	-233	Ø	505	-523
6	157	145	3	255	-255	I	299	-302	I	36	13
7	374	383	4	157	150	2	183	-190	2	319	-320
8	-36	11	5	317	-314	3	383	-387	3	343	327
9	172	172	6	133	-115	4	250	-256	4	186	-192

Segue: TABLE III.

5	361	368	8	60	-72	-10	165	133	4	157	175
6	165	141	9	64	64	-9	-31	-16	5	39	45
7	154	147	10	39	-41	-8	180	153	6	188	178
8	-36	-16	11	-23	16	-7	114	-112	7	93	73
9	183	205				-6	183	183	8	106	90
10	78	78	2	12	L	-5	139	-140	9	-10	-3
11	75	58	-13	72	-68	-4	139	122			
12	60	61	-12	-26	26	-3	244	-240	2	17	L
			-11	98	-87	-2	108	90			
2	10	L	-10	217	207	-1	376	-410	-9	85	-86
-14	-18	-8	-9	-36	9	0	118	-92	-8	64	59
-13	62	-56	-8	51	22	1	240	-260	-7	186	-167
-12	115	-128	-7	62	51	2	118	-96	-6	-31	51
-11	-33	34	-6	51	31	3	186	-200	-5	152	-122
-10	106	-116	-5	57	39	4	168	-173	-4	114	119
-9	-36	-36	-4	72	66	5	-36	-29	-3	67	-60
-8	350	-370	-3	347	389	6	160	-178	-2	96	97
-7	219	226	-2	190	192	7	-31	-17	-1	60	57
-6	304	-342	-1	301	304	8	42	-34	0	142	142
-5	-33	3	0	49	-41	9	28	33	1	42	35
-4	229	-212	1	296	320	10	-18	-26	2	136	140
-3	133	115	2	180	-184				3	144	146
-2	208	-202	3	51	-19	2	15	L	4	67	72
-1	240	227	4	139	-125	-11	-21	-11	5	160	139
0	157	135	5	108	111	-10	88	72	6	-26	19
1	190	187	6	142	-133	-9	-28	-44	7	51	62
2	250	247	7	62	-66	-8	-31	-20			
3	281	256	8	90	-92	-7	62	-60	2	18	L
4	512	515	9	144	-128	-6	118	-133	-9	-13	-11
5	-36	-3	10	-26	15	-5	44	-41	-8	-21	12
6	152	148	11	75	-76	-4	412	-437	-7	108	97
7	36	36				-3	78	-72	-6	-26	17
8	170	181	2	13	L	-2	263	-254	-5	170	147
9	-33	8	-12	-23	31	-1	62	63	-4	-28	-4
10	100	89	-11	162	142	0	355	-379	-3	250	218
11	-26	10	-10	54	-69	1	-36	28	-2	-31	10
12	-18	-6	-9	250	219	2	250	-257	-1	291	238
			-8	75	80	3	-36	36	0	44	60
2	11	L	-7	263	264	4	103	-113	1	168	146
-13	-23	-14	-6	-36	29	5	-33	23	2	-28	4
-12	118	-87	-5	240	237	6	-31	-5	3	154	135
-11	98	-86	-4	44	28	7	69	61	4	-26	22
-10	93	-102	-3	214	200	8	67	48	5	33	48
-9	80	-67	-2	188	174	9	93	75	6	-21	-4
-8	133	139	-1	199	-188				7	-13	-29
-7	-36	-23	0	124	115	2	16	L			
-6	289	286	1	310	-314				2	19	L
-5	139	-122	2	88	71	-10	165	-170	-7	82	88
-4	386	393	3	168	-155	-9	-26	12	-6	-21	12
-3	129	100	4	57	42	-8	217	-189	-5	114	104
-2	482	486	5	258	-266	-7	-31	14	-4	114	90
-1	80	-63	6	-36	-31	-6	253	-202	-3	-26	24
0	400	408	7	199	-212	-5	90	-79	-2	160	143
1	196	192	9	193	-186	-3	49	-31	-1	-28	33
2	317	330	10	-23	-12	-2	-36	-8	0	115	115
3	281	281				-1	67	54	1	46	-60
4	98	86	2	14	L	0	72	-65	2	36	39
5	62	45				1	85	-91	3	57	-57
6	118	131	-12	57	53	2	247	235	4	-21	17
7	129	110	-11	-23	-17	3	-33	-28	5	118	-135

Segue: TABLE III.

2	20	L	-13	-25	-19	-13	-31	6	-13	52	-66
-5	67	-71	-12	41	-42	-12	98	-120	-12	167	138
-4	93	83	-11	93	-84	-11	142	161	-11	-36	-6
-3	85	-85	-10	121	-120	-10	258	-258	-10	152	151
-2	-23	4	-9	279	-303	-9	395	426	-9	70	-58
-1	60	-52	-8	108	105	-8	230	-237	-8	309	311
0	96	-91	-7	429	-477	-7	369	388	-7	230	224
1	62	-56	-6	-18	5	-6	163	-147	-6	-31	-30
2	142	-131	-5	482	-507	-5	237	248	-5	243	239
3	46	-56	-4	76	69	-4	129	128	-4	196	-195
3	0	L	-3	302	-369	-3	189	197	-3	160	176
3	0	L	-2	258	255	-2	196	199	-2	309	-327
-14	117	125	-1	256	-282	-1	336	325	-1	83	86
-12	117	109	0	157	150	0	292	319	0	217	-203
-10	237	258	1	186	-182	1	111	116	1	-29	-26
-8	240	225	2	178	182	2	289	279	2	452	-448
-6	33	27	3	273	275	3	160	-136	3	83	-79
-6	160	-131	4	160	146	4	356	351	4	503	-477
*-2	207	-449	5	183	168	5	111	-99	5	155	-135
0	441	-489	6	258	253	6	70	-38	6	163	-165
2	384	-404	7	201	199	7	180	-173	7	176	-167
4	372	-343	8	44	50	8	-36	25	8	86	-72
6	286	-281	9	-33	41	9	98	-101	9	52	-59
8	170	-166	10	-33	28	10	-31	-15	10	-31	-23
10	-33	46	11	132	122	11	52	-53	11	-26	21
12	-23	21	12	-23	-36	12	-20	-2	12	-18	0
3	1	L	3	3	L	3	5	L	3	7	L
-15	47	48	-15	70	-63	-15	-20	-9	-14	-23	-14
-14	70	60	-14	-22	-13	-14	-26	-3	-13	129	120
-13	136	134	-13	137	-156	-13	-31	17	-12	-31	30
-12	65	-70	-12	78	-88	-12	86	99	-11	111	124
-11	147	155	-11	250	-300	-11	-36	-26	-10	-36	8
-10	65	-68	-10	146	-160	-10	93	104	-9	-36	10
-9	94	87	-9	127	123	-9	144	164	-8	49	41
-8	340	-335	-8	183	-195	-8	317	345	-7	289	285
-7	65	48	-7	61	-60	-7	59	-60	-6	307	-315
-6	218	-231	-6	226	-209	-6	485	543	-5	212	-184
-5	334	-298	-5	-17	20	-5	157	157	-4	279	-240
-4	756	-828	-4	222	-238	-4	546	624	-3	397	-406
-3	84	-62	-3	436	470	-3	93	-71	-2	152	-155
-2	307	-369	-2	41	33	-2	580	697	-1	395	-405
-1	452	-512	-1	526	632	-1	119	119	0	190	-183
0	206	-193	0	232	-235	0	73	62	1	418	-409
1	420	-435	*1	730	863	1	235	-199	2	137	-124
2	167	156	2	193	-176	2	201	180	3	325	-331
3	350	-339	3	304	320	3	-29	-18	4	-33	-35
4	119	113	4	116	101	4	134	-122	5	212	-216
5	193	-191	5	253	244	5	193	201	6	111	90
6	189	188	6	83	75	6	157	-141	7	126	-129
7	77	-62	7	44	32	7	57	51	8	-33	-36
8	243	262	8	44	53	8	155	-162	9	-31	1
9	-33	3	9	-33	3	9	-33	18	10	-29	26
10	119	127	10	-31	5	10	119	-97	11	-23	19
11	-29	50	11	-29	-34	11	-26	-25	12	-16	4
12	41	44	12	46	49	12	41	-35	3	8	L
3	2	L	3	4	L	3	6	L	-14	-20	2
-15	-18	24	-15	-20	14	-15	-18	20	-13	-29	-5
-14	76	-70	-14	86	-63	-14	178	173	-12	-31	28

Segue: TABLE III.

—II	155	—138	—6	147	115	I	—36	46	3	15	L
—IØ	—36	52	—4	—33	27	2	214	—201	—II	—16	—15
—9	224	—233	—3	158	143	3	—36	—19	—IØ	111	—110
—8	49	47	—2	408	388	4	44	—29	9	—26	—22
—7	312	—351	—1	—33	—51	5	100	—100	8	232	—196
—6	157	—155	Ø	508	533	6	98	—80	7	—31	30
—5	555	—617	1	126	—116	7	126	—104	6	201	—169
—4	—31	—18	2	415	407	8	77	—70	5	—33	51
—3	268	—242	3	—33	31	9	103	—94	4	196	—193
—2	36	—25	4	273	264	10	—16	—40	3	—33	19
—1	266	—268	5	173	—163				2	111	—98
Ø	124	—115	6	134	139				1	178	168
I	—31	—4	7	41	40	3	13	L	Ø	121	—131
2	157	—157	8	49	49	—12	54	53	I	—33	—16
3	134	115	9	75	—76	—11	113	88	2	103	98
4	100	—83	10	—23	—15	—10	67	—70	3	67	80
5	299	293	11	—16	—19	—9	190	174	4	96	80
6	186	188				—8	—33	—16	5	86	69
7	243	236				—7	—33	21	6	150	145
8	—33	—11	3	11	L	—6	—36	8	7	59	50
9	173	158	—13	59	—49	—5	—36	—18	8	44	89
10	—29	30	—12	62	—25	—4	—36	22			
11	73	62	—11	152	—118	—3	206	—172	3	16	L
			—10	209	202	—2	—36	—24			
3	9	L	—9	49	—55	—1	193	—166	—10	44	—76
—14	—18	35	—8	183	184	Ø	152	—149	—9	—20	—29
—13	62	—52	—7	—36	—63	I	247	—240	—8	49	—31
—12	41	—33	—6	323	322	2	—36	—20	7	67	—53
—11	137	113	—5	196	—186	3	219	—219	6	—29	—31
—10	144	—120	—4	144	134	4	124	—122	5	116	—83
—9	132	—111	—3	83	66	5	144	—137	4	86	72
—8	245	—249	—2	338	333	6	57	—54	3	—31	—44
—7	70	68	—1	121	105	7	86	—75	2	176	158
—6	155	—156	Ø	183	178	8	—23	21	—1	62	—67
—5	98	88	1	190	161	9	—18	Ø	Ø	193	197
—4	227	—224	2	93	91				I	—31	26
—3	186	161	3	100	—101				2	190	209
—2	333	—345	4	113	—101	3	14	L	3	—29	4
—1	346	323	5	87	72				4	113	110
Ø	—31	—6	6	96	—94	—12	—10	—12	5	49	44
I	253	228	7	86	79	—11	52	—37	6	93	83
2	103	95	8	98	—72	—10	75	75	7	—16	41
3	279	264	9	73	—60	—9	137	—101			
4	160	144	10	83	—83	—8	—31	44	3	17	L
5	160	149				—7	152	—154			
6	77	77				—6	—33	—15	—9	49	—100
7	59	68	3	12	L	—5	180	—187	—8	98	94
8	—33	53	—13	—16	9	—4	190	—181	—7	—23	—26
9	41	—53	—12	98	93	—3	330	—335	—6	150	120
10	147	134	—11	106	99	—2	209	—214	—5	—29	21
11	—18	—7	—10	—31	38	—1	142	—136	—4	157	130
			—9	129	99	Ø	160	—150	—3	83	68
3	10	L	—8	90	79	I	54	60	—2	36	33
—13	62	51	—6	160	163	2	260	—263	I	186	143
—12	183	—156	—5	392	385	3	—33	—Ø	Ø	132	122
—11	62	76	—4	86	—69	4	70	—73	I	121	106
—10	247	—229	—3	325	319	5	—31	24	2	—29	—8
—9	—36	47	—2	59	—64	7	77	65	3	180	177
—8	126	—96	—1	212	194	8	—20	20	5	90	73
—7	134	126	Ø	214	—216	9	—16	85	6	—16	—37

Segue: TABLE III.

3	18	L	2	225	217	4	70	89	6	190	-208
-8	-13	-13	3	62	-67	5	-50	26	7	-47	-55
-7	126	125	4	112	98	6	-50	1	8	70	-86
-6	-20	-13	5	-50	24	7	-50	-17	9	-38	-23
-5	165	151	6	147	150	8	-47	26	10	-31	-50
-4	-26	5	7	-50	56	9	-43	-36	11	-20	26
-3	157	140	8	70	80	10	-35	7			
-2	93	79	9	-43	-17	11	-23	-32	4	6	L
-1	87	68	10	-35	-16						
0	-26	-12	11	-27	11	4	4	L	-14	31	37
1	90	83				-15	-23	-18	-13	-38	2
2	-23	-33	4	2	L	-14	-35	-41	-12	-43	51
3	-20	-10	-15	-27	-1	-13	58	69	-10	-50	-17
4	-18	-14	-14	62	-61	-12	-47	1	-9	81	74
			-13	97	-89	-11	120	101	-8	62	-29
3	19	L	-12	55	49	-10	-50	-43	-7	341	323
-6	52	112	-11	267	-245	-9	-50	59	-6	279	-280
-5	-18	-15	-10	88	-101	-8	275	256	-5	78	86
-4	119	94	-9	225	-221	-7	66	-55	-4	353	-334
-3	121	-111	-8	73	56	-6	341	324	-3	78	-55
-2	-20	31	-7	205	-184	-5	178	144	-2	376	-380
-1	103	-96	-6	76	49	-4	376	396	-1	58	-54
0	-20	9	-5	100	29	-3	85	84	0	310	-307
1	132	-131	-4	100	67	-2	337	360	1	193	-179
2	-18	-32	-3	89	-75	-1	47	-37	2	186	-182
3	49	-105	-2	186	174	0	260	271	3	-47	-20
			-1	38	32	1	186	-162	4	135	-137
4	0	L		210	190	2	302	303	5	201	-217
-14	112	113	2	97	93	3	190	-214	6	105	112
-12	76	89	3	217	212	5	-50	-45	7	-47	31
-10	-35	-2	4	-47	11	6	-50	12	8	-43	21
-8	353	-359	5	248	252	7	58	-70	10	38	54
-6	236	-184	6	-50	52	8	-47	-58			
-4	517	-542	7	97	114	9	-43	-23			
0	302	-317	8	-47	-79	10	43	-54	4	7	L
2	406	-446	9	81	101	11	-23	-45	-14	-27	-50
4	78	-52	10	-35	-49				-13	-35	51
6	-50	-22	11	-27	27	4	5	L	-12	73	-88
8	132	187				-15	-20	-29	-11	-47	28
10	55	86	4	3	L	-14	108	108	-10	58	-60
						-13	-38	21	-8	298	-269
4	1	L	-15	47	-56	-12	155	119	-7	85	-75
-15	-27	10	-14	81	-79	-11	70	61	-6	112	-109
-14	132	-118	-13	78	-79	-10	225	216	-5	388	-392
-13	120	112	-12	66	77	-9	210	-206	-4	-47	-14
-12	88	-100	-10	-35	-19	-8	275	262	-3	233	-213
-11	46	-56	-9	-35	-18	-7	58	-77	-2	112	115
-10	245	-271	-8	71	70	-6	360	333	-1	271	-265
-9	32	17	-7	280	275	-5	-43	-4	0	89	92
-8	362	-370	-6	105	-104	-4	-38	23	1	155	-144
-7	-29	-20	-5	295	287	-3	143	-127	2	158	171
-6	389	-345	-4	58	39	-2	182	-160	3	170	-174
-5	190	-153	-3	372	390	-1	78	-70	4	175	170
-4	286	-292	-2	38	8	0	228	-217	5	-50	-27
-3	187	-275	-1	318	321	1	58	-48	6	124	155
-2	182	168	0	93	50	2	175	-178	7	81	111
-1	298	-249	1	228	249	3	89	84	8	62	83
0	120	108	2	120	127	4	406	-415	9	55	86
1	-35	13	3	66	-69	5	-50	-24	10	-27	27

Segue: TABLE III.

4	8	L	-6	217	193	5	116	98	2	163	155
-14	38	22	-5	-50	-23	6	-38	-31	3	-38	47
-13	78	-77	-4	205	219	7	112	-107	4	73	72
-12	50	50	-3	-50	33	8	-23	30	5	-27	9
-11	120	-113	-2	321	302				6	-20	41
-10	-47	-9	-1	-50	3	4	13	L			
-9	228	-227	Ø	240	252	-11	-27	-8	4	16	L
-8	128	-134	1	128	125	-10	-35	-21	-9	-15	-58
-7	275	-270	2	55	29	-9	47	-61	-8	-27	45
-6	-50	45	3	-50	40	-8	-43	59	-7	55	-60
-5	198	-191	4	-50	1	-7	158	-132	-6	124	129
-4	62	59	5	-47	-13	-6	-47	-29	-5	-38	-7
-3	-47	-18	6	55	-69	-5	175	-147	-4	190	163
-2	198	-202	7	-38	43	-4	-47	-7	-3	-38	1
-1	58	51	8	-35	28	-3	260	-287	-2	147	120
Ø	-47	-25	9	-23	-8	-2	93	-93	-1	-38	-Ø
1	116	106				-1	248	-259	Ø	167	156
2	70	79	4	11	L	Ø	-47	-5	1	-38	-2
3	186	169				1	135	-139	2	62	66
4	132	146	-13	-15	-28	2	-47	10	3	62	78
5	66	51	-12	143	152	3	66	-73	4	-27	2
6	-47	-39	-11	-38	20	4	-43	Ø	5	-15	39
7	70	67	-10	193	175	5	-38	-40			
8	-38	-25	-9	-47	26	6	-35	20			
9	-35	-19	-8	108	94	7	38	41	4	17	L
10	-23	32	-7	73	74				-7	43	65
			-6	151	121				-6	-27	27
4	9	L	-5	228	221	4	14	L	-5	132	125
-13	-31	24	-4	101	104	-11	-15	-25	-4	-35	32
-12	120	-95	-3	193	163	-10	-27	39	-3	116	113
-11	-43	-12	-2	73	74	-9	128	-112	-2	78	71
-10	132	-127	Ø	198	-219	-8	62	-68	-1	147	145
-9	73	80	1	105	113	-7	140	-122	Ø	-35	-18
-8	158	-134	2	213	-223	-6	-43	-23	1	73	73
-7	66	47	3	-50	46	-5	55	-59	2	-27	-45
-6	-50	11	4	167	-170	-4	97	-90	3	-23	20
-5	263	250	5	-47	40	-3	-47	32			
-4	140	-114	6	97	-106	-2	58	-42			
-3	186	165	7	62	-66	-1	143	122	4	18	L
-2	-47	35	8	101	-115	Ø	58	-52			
-1	213	211	9	-15	-37	1	-47	30	-5	-23	73
Ø	147	128				2	-43	-33	-4	-23	-8
1	147	129	4	12	L	3	93	103	-3	-27	10
2	135	144				4	-38	15	-2	55	-70
3	124	116	-12	73	90	5	112	105	-1	38	-60
4	128	124	-11	105	81	6	-35	35	Ø	-23	-21
5	-50	-41	-10	-38	-43				1	50	-69
6	66	77	-9	167	162	4	15	L	2	-8	-25
7	66	-23	-8	-47	-67						
8	85	91	-7	143	147	-10	-20	-78	5	Ø	L
9	-31	-5	-6	112	-120	-9	-27	-5			
			-5	62	63	-8	112	-104	-14	95	-91
4	10	L	-4	170	-170	-7	-38	33	-12	37	-34
-13	-23	-1	-2	158	-154	-5	-43	-14	-10	132	-140
-12	120	-113	-1	105	-108	-4	116	-96	-8	215	-206
-11	-38	17	Ø	163	-162	-3	-43	-2	-6	186	-140
-10	-43	29	1	151	-145	-2	55	70	-4	256	-327
-9	-47	26	2	-50	-19	-1	-43	20	-2	95	-64
-8	70	62	3	151	-155	Ø	-43	28	2	209	226
-7	70	73	4	55	-73	1	-43	43	4	130	137

Segue: TABLE III.

6	65	82	-8	-55	-22	3	-55	35	-10	80	-73
8	90	84	-7	244	232	4	90	-67	-9	-55	-19
			-6	-50	-29	5	139	-148	-8	-55	11
5	1	L	-5	215	203	6	-50	33	-7	-55	35
-14	-30	-23	-4	55	59	7	-45	-28	-6	-55	31
-13	-45	-38	-2	105	96	8	-40	19	-5	150	163
-12	85	-70	-1	80	47				-4	85	-85
-11	-55	-29	Ø	50	-28	5	6	L	-3	209	229
-10	95	-99	1	-50	-19	-13	55	39	-2	-55	-21
-9	120	-118	2	114	98	-12	75	-63	-1	194	184
-8	62	72	3	-55	-2	-11	-50	31	Ø	-55	31
-7	277	-245	4	-55	26	-10	99	-95	1	190	180
-6	260	261	5	55	-45	-9	-55	22	2	55	48
-5	173	-143	6	-55	-22	-8	225	-223	3	175	182
-4	210	256	7	60	-65	-7	-55	8	4	190	-85
-2	334	358	8	-40	-5	-6	274	-272	5	135	134
-1	169	-162				-5	209	-228	6	-45	-35
Ø	145	111				-4	120	-77	7	-35	23
1	75	77	5	4	L	-3	65	-56	8	25	25
2	284	268	-14	-25	34	-2	85	-68			
3	-55	11	-13	75	63	-1	120	-110	5	9	L
4	90	87	-12	-45	7	Ø	-55	2	-12	75	-84
5	55	45	-11	110	73	1	80	-60	-11	-40	19
6	85	88	-10	175	163	2	-55	43	-10	-45	-11
7	50	48	-9	95	82	3	70	-72	-9	50	51
8	-45	-9	-8	80	62	4	105	129	-8	-55	-10
			-7	55	32	5	-55	-45	-7	99	105
5	2	L	-6	145	133	6	110	121	-6	-55	-47
-14	-30	-43	-5	90	75	7	-45	11	-5	145	160
-13	225	-214	-4	240	220	8	-35	53	-4	-55	-14
-12	50	69	-3	105	-101				-3	125	123
-11	-55	-29	-1	120	-126	5	7	L	-2	154	141
-10	55	48	Ø	-50	29				-1	70	65
-9	95	-86	1	209	-212	-13	35	-46	Ø	164	172
-8	120	123	2	-55	-47	-12	50	-47	1	70	59
-7	108	-90	3	-55	-42	-11	-45	14	2	90	77
-6	66	50	4	70	-66	-10	-50	-22	3	-55	-9
-5	82	-69	5	60	-42	-9	110	-110	4	50	38
-4	140	141	6	50	-61	-8	65	-52	5	-45	-35
-3	-21	12	7	65	-73	-7	204	-197	6	-40	11
-2	70	63	8	40	-16	-6	-55	30	7	-30	-7
-1	334	349				-5	225	-226			
Ø	60	-69	5	5	L	-4	85	108	5	10	L
1	135	113				-3	110	-83			
2	-55	11	-13	-40	-3	-2	-55	33	-12	-25	77
3	125	109	-12	45	44	-1	139	-133	-11	-35	30
4	70	-84	-11	-50	-2	Ø	-55	33	-10	194	176
5	80	45	-10	154	124	1	-55	11	-9	-50	-14
6	75	-73	-9	-55	-16	2	-55	-5	-8	160	138
7	-50	28	-8	80	69	3	-55	58	-7	-55	30
8	40	-52	-7	85	69	4	80	76	-6	164	164
			-6	60	-68	5	135	149	-5	-55	-21
5	3	L	-5	55	34	6	-45	-49	-4	145	136
-14	-30	6	-4	229	-244	7	-40	58	-3	-55	-6
-13	-40	-1	-3	120	-123	8	35	-56	-2	154	130
-12	-50	-17	-2	135	-133				-1	-55	2
-11	164	142	Ø	215	-204	5	8	L	Ø	-55	-57
-10	90	-77	1	75	-67	-12	-35	26	2	55	-76
-9	164	159	2	240	-197	-11	125	-119	3	50	-52

Segue: TABLE III.

4	55	-47	5	12	L	-6	-45	13	1	60	69
5	55	-67	-10	70	-91	-5	80	-87	2	-40	13
6	-35	-20	-9	45	40	-4	-50	-24	3	55	61
7	-25	-25	-8	80	-59	-3	110	-117			
			-7	-50	-45	-2	-50	43	5	15	L
			-6	60	-71	-1	-50	-8	-7	-30	-18
5	11	L	-5	65	-81	Ø	-50	39	-6	-35	21
-11	-30	25	-4	-55	-37	1	-45	-18	-5	45	70
-10	70	44	-3	105	-134	2	-45	-17	-4	60	66
-9	-45	38	-2	75	-73	3	-40	37	-3	-40	43
-8	-50	-11	-1	120	-125	4	-35	-7	-2	90	105
-7	80	Ø	-50	23	5	25	63		-1	-40	63
-6	60	64	1	120	-129				Ø	70	70
-5	-55	7	2	-50	21				1	-35	9
-4	75	-101	3	-45	-36	5	14	L	2	65	94
-3	-55	38	4	-40	23	-9	-20	-67			
-2	85	-100	5	-35	-43	-8	70	-80			
-1	-55	-17	6	-10	22	-7	-40	10	5	16	L
Ø	190	-210				-6	55	-56	-5	35	32
1	-55	-6				-5	-45	32	-4	65	85
2	-50	-31	5	13	L	-4	99	-89	-3	-40	46
3	70	-81	-10	-20	40	-3	-45	34	-2	45	54
4	-55	-46	-9	65	-62	-2	-45	-48	-1	50	83
5	40	-39	-8	-40	17	-1	-45	48	Ø	-25	19
6	-30	-32	-7	160	-167	Ø	-45	-11	1	-20	68

TABLE IV.
Average planes in the molecule.

	q_a	q_b	q_c	d	ϑ
Ring <i>trans</i> to Br	-0.3640	-0.6510	0.7334	2.826	70.7
Ring <i>cis</i> to Br	0.5774	0.4238	0.5413	3.929	47.2
Molecular skeleton ...	0.7485	-0.3472	0.3716	0.016	

q_a, q_b, q_c = direction cosines of the plane normal (relative to the crystallographic axes); d = distance from the origin (\AA); ϑ = dihedral angle with the molecular skeleton plane (degrees).

In fig. 3 the packing in the crystal is viewed along the α axis. Using the following Van der Waals radii: C = 1.7, Br = 1.95, CH₃ = 2.0 Å, no intermolecular distances significantly shorter than the touching distances were found. Considering also the hydrogen atoms in the calculated positions, with a Van der Waals radius of 1.2 Å, only three contacts appear significantly shorter than the touching distance. In two of them the same hydro-

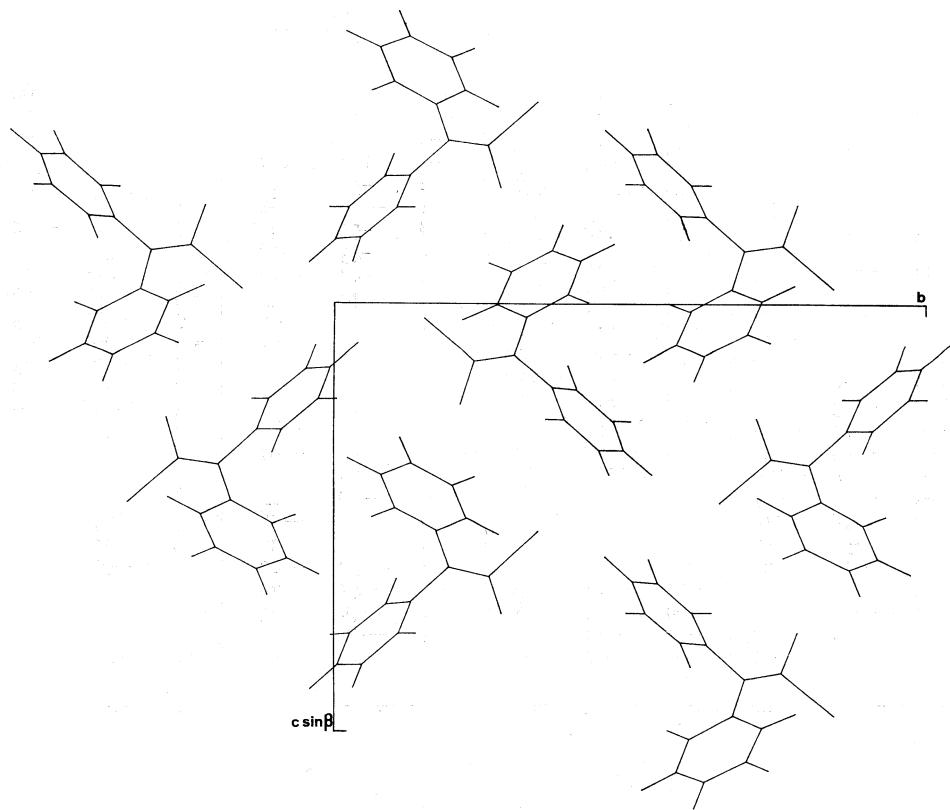


Fig. 3. - The crystal structure viewed along the α axis.

gen atom is involved, compressed between a bromine atom and a methyl group:

Atom in x, y, z	with atom	in position	Distance (\AA)
C (1)	H (3)	$-1 + x, 1/2 - y, 1/2 + z$	3.115
H (2)	Br	$1 + x, y, z$	2.964
H (2)	C (1)	$1 + x, 1/2 - y, -1/2 + z$	3.030

DISCUSSION.

With respect to the structure of 2-bromo-1,1-di-*p*-tolylethylene [1], the most striking difference in 2-bromo-1,1-diphenyl-prop-1-ene is the increased value for the rotation angle of the ring in *trans* with the bromine atom (from 24.4° to 70.7°). This is related to the large steric hindrance of the methyl group. Correspondingly, the rotation angle for the *cis* ring decreases from 67.9° to 47.2° . Both the carbon-bromine and carbon-methyl distances are

significantly larger than in [1], while the C(1)-C(2)-Br angle is quite small (110.5°); the ethylenic bond shows a significant shortening. Calculations are in progress to check if this conformation can be explained, as in the bromo-ditolylethylene compound, as corresponding to a minimum of the "total" energy, considering the π -electron, bending, stretching and steric repulsion contributions for an isolated molecule of our compound and in the corresponding model crystal.

The e.s.d.'s on the bond lengths and bond angles result considerably lower than for the bromo-ditolylethylene compound but they seem to be underestimated also in this case. Here, the absence of an absorption correction however appears to be more reasonable, because of the size of the crystal used. The thermal motion is remarkably large, with a pronounced anisotropy for Br, C(7) and C(13).

All the calculations except the full-matrix least-squares refinement were performed on an IBM 1620-20K electronic computer. Structure factors, Fourier syntheses and isotropic block-diagonal least-squares were calculated using available programs [11, 12, 13]. The intensity scaling and correction program has been written by Gramaccioli and Mariani [4]. The final cycles of least-squares refinement were carried on a IBM 7040 electronic computer, using a slightly modified version of the OR-FLS program [14].

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